



8 W Auxiliary Power for White Goods and Industrial Equipment with FSL518APG

EVAL BOARD USER'S MANUAL

Table 1. GENERAL SPECIFICATIONS

Devices	Applications	Input Voltage	Output Power	Topology	Board Size
FSL518APG	White Goods and Industrial Power Supplies	90–265 Vac	8 W	Isolated Flyback	80 × 38 × 20 mm 2.15 W/inch ³
Output Spec.	Turn on Time	Efficiency	Operating Temperature	Cooling	Standby Power
12 V/0.66 A	< 200 ms	Above 85% @ Full Load	0–50°C	Open Frame in Still Air	< 50 mW @ 230 Vac

Description

This user manual provides elementary information about an isolated flyback with FSL518APG, it performs high efficiency and smaller than 50 mW no-load power consumption. FSL518APG is an integrated pulse width modulation (PWM) and 800 V power switch with SENSEFET®, it can help to save external MOSFET and sense resistor, increase power density and reliability. This application is targeting auxiliary power supply for white goods and industrial equipment, such as refrigerator, E-metering or similar types of equipment.

The PWM controller includes an integrated variable frequency oscillator, Under-Voltage Lockout (UVLO), Leading Edge Blanking (LEB), optimized gate driver, internal soft-start, and temperature-compensated precise current source for loop compensation and self-protection circuitry. This design focuses mainly on the FSL518APG current-mode PWM controller. Please refer to FSL518APG's materials to get more information about this device.

The FSL518APG is a current-mode PWM controller, it can have better response to handle dynamic operation. Controller combines line detection and burst-mode adjustment in one pin. It's easy to achieve these functionalities just need voltage divider and one Zener diode. Line detection includes brown-in, brown-out and line OVP, burst-mode adjustment is for fine tune audible noise and light load efficiency. Of course, it also provides frequency reduction with loading decreasing for gaining more design margin to improve light load efficiency.

Key Features

- Integrated Rugged 800 V Super Junction MOSFET with SENSEFET Technology
- Built-in HV Current Source for Start-up
- Peak-Current-Mode Control with Slope Compensation
- Line Compensation for Maximum Over-Power Limiting
- Advanced Soft-start for Low Electrical Stress
- Peak-Current-Mode Control with Built-in Slope Compensation
- Pulse-by-pulse Current Limit
- Line Brown-in, Brown-out, and Over-Voltage Protection (LOVP)
- Adjustable Burst-mode Operation
- Frequency Hopping for Better EMI
- Various Protections:
 - ◆ Auto Restart Mode: Brown-out, OLP, OVP, AOCV and TSD
 - ◆ Recovery Immediately by Triggering Level: LOVP

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DETAIL DEMO-BOARD SCHEMATIC DESCRIPTION

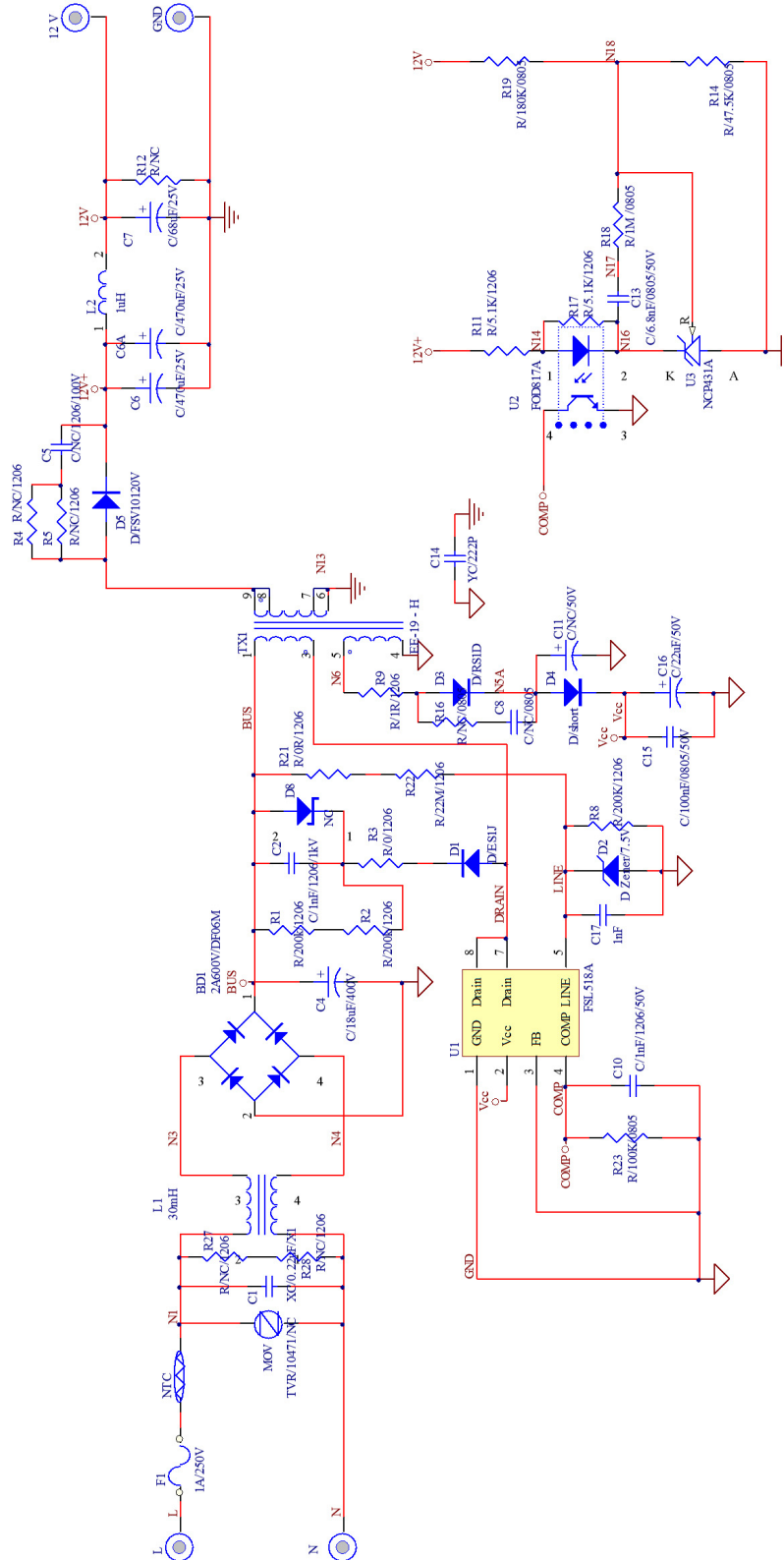


Figure 1. FSL518AFLYGEVB Demo-Board – Main Board Schematic

The input EMI filter is formed by components L1 and C1. Bleeder for X-cap, R27 and R28, are left not connected.

The primary side of flyback converter is composed of these devices; power transformer TX1, dc-link capacitor, TVS snubber, the integrated switcher U1 (FSL518APG) and related components. Meanwhile, the integrated switcher has a peak current mode PWM controller and 800 V super junction MOSFET. D1, R3 and D8 form TVS snubber to protect instant voltage spike produced by leakage inductance. The FB pin of U1 needs to connect to reference ground due to isolated flyback already exists regulator as NCP431A so that don't need to employ internal error amplifier. U2 couples the reactive current of U3 to primary side and connect to COMP pin, the coupled current and internal sourcing current is converted to control voltage of PWM for output voltage regulation, R23 and C10 can be used for adjusting response of feedback signal. LINE pin of U1 connects voltage divider from bulk capacitor to detect input voltage for some protections of brown-in, brown-out and LOVP. Besides, there is parallel-connected D2 on LINE pin to adjust burst threshold to fine tune audible noise and light load efficiency. C17 is used to avoid larger switching

noise interference, which is usually recommended around 1 nF~3.3 nF. Auxiliary winding shares same ground reference with U1. That is, reference ground is negative terminal of output of bridge rectifier BD1. Transformer winding is also used for providing VCC voltage in normal operation. R9 and D3 provide path to delivery energy when PWM is turned off. C16 can keep enough voltage if PWM is turned off for a while, and C15 is for better stability.

The secondary-side output is mainly composed of D5, C6 and C6A. When the MOSFET integrated in the switcher turns off, energy stored in the coupled inductor is transferred to the secondary side. At the time, there is switching noise on the output voltage, which can be, however, reduced by a LC filter on each output terminal formed by L2 and C7. U3 is a shunt regulator, and output is taken into account for generating feedback signal with network formed by R19 and R14. R18, C13, and R11 are used to adjust feedback response and bias U3. R17 provides additional biasing current for U3 to keep its required operating current. Cathode current of U3 is coupled to primary side by an opto-coupler, U2.

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CIRCUIT LAYOUT

The PCB consists of a double layer FR4 board with 2 oz. copper cladding.

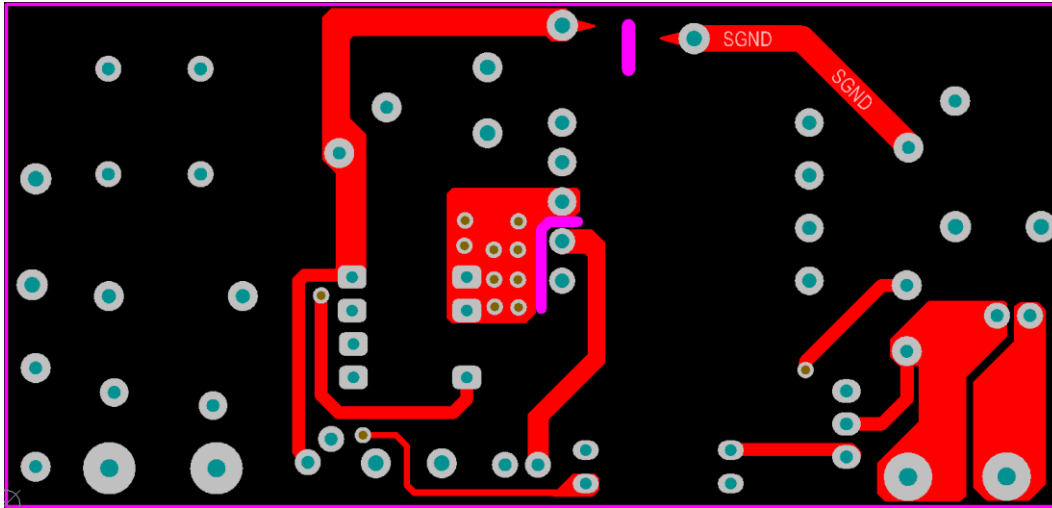


Figure 2. Main Board Top Layer

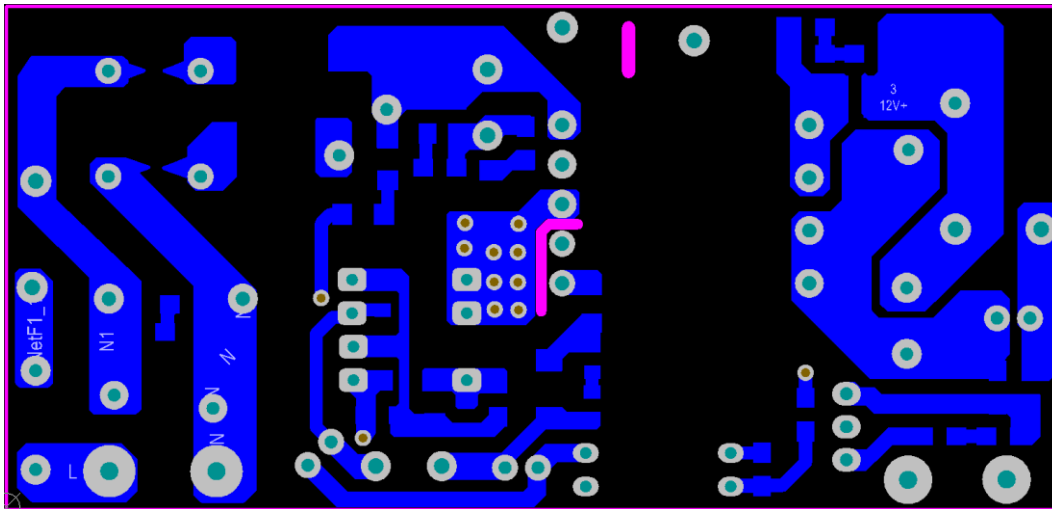


Figure 3. Main Board Bottom Layer

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CIRCUIT LAYOUT (Continued)

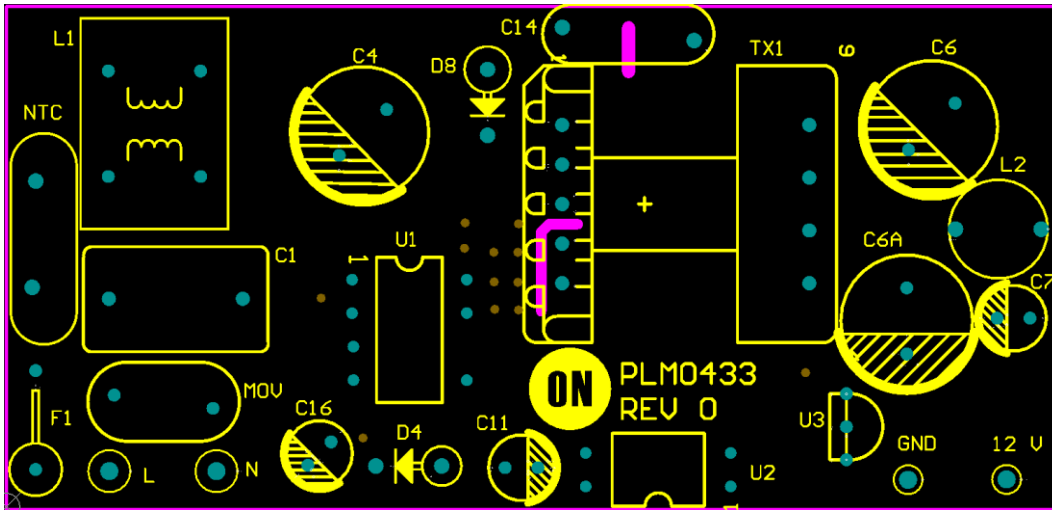


Figure 4. Main Board Top Side Components

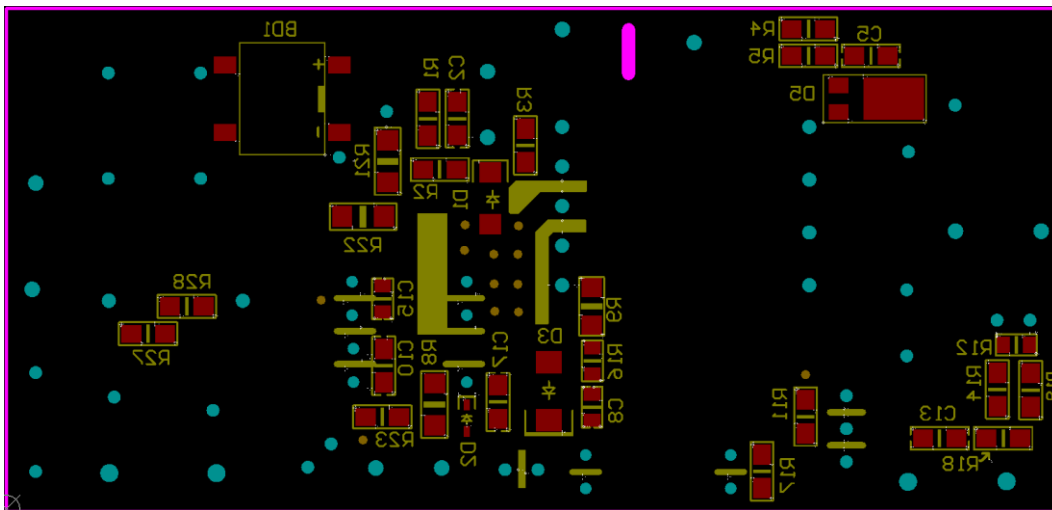


Figure 5. Main Board Bottom Side Components

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BOARD PICTURES

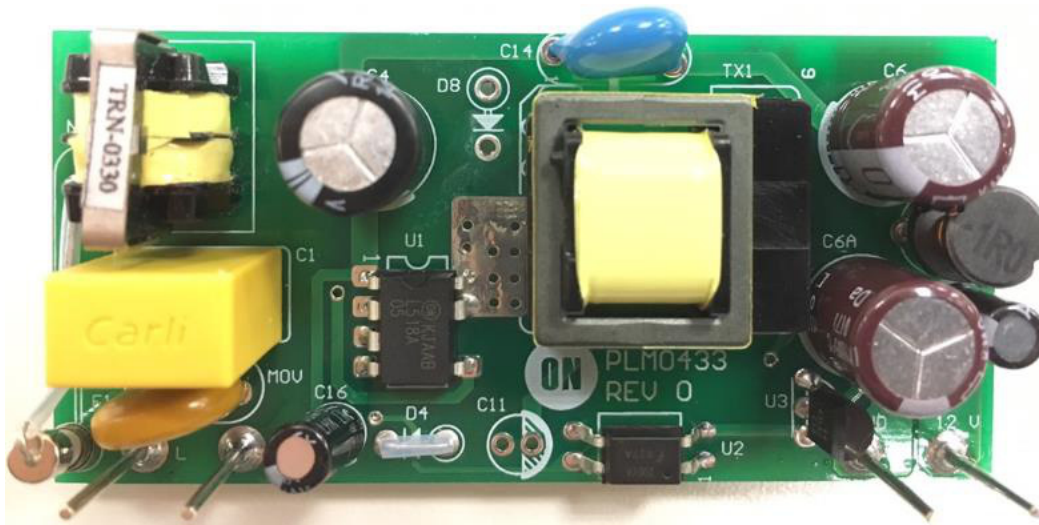


Figure 6. Main Board Photo – Top Side

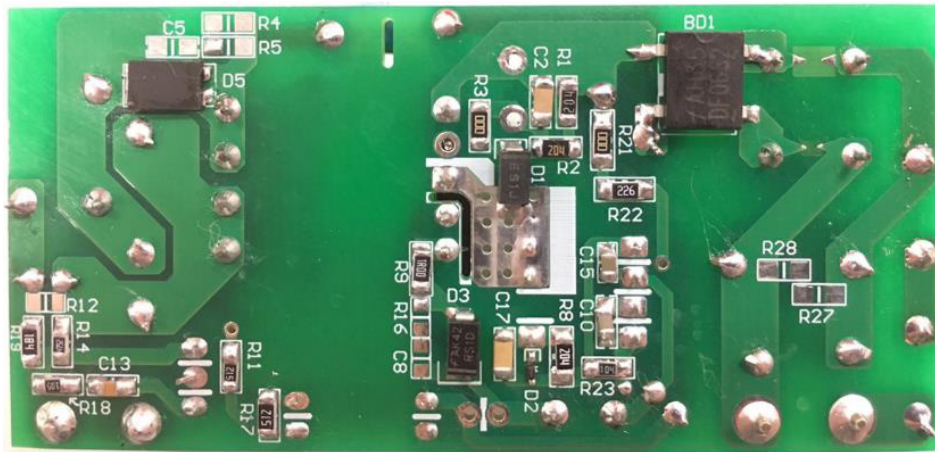


Figure 7. Main Board Photo – Bottom Side

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TRANSFORMER DATA

Bobbin & Core : EE-19-H-9P

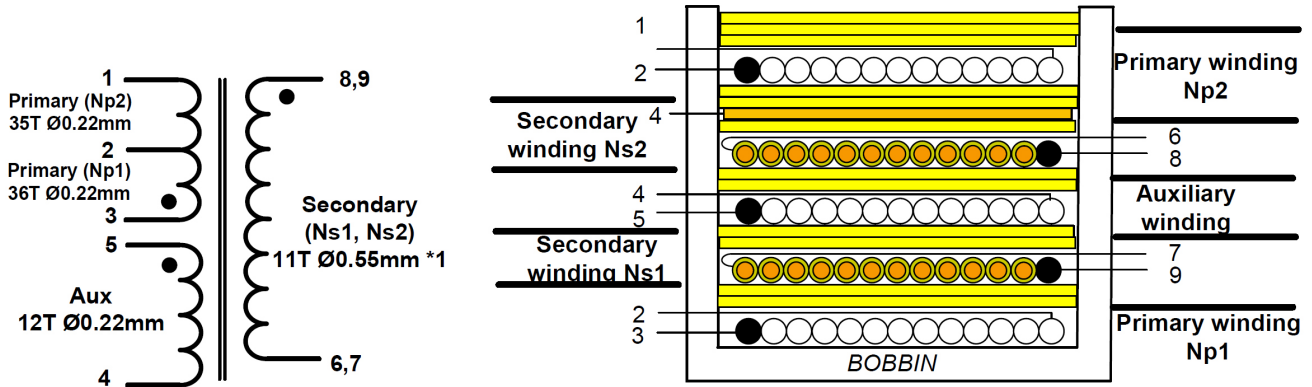


Table 2.

	Pin	Specification	Remark
Primary-Side Inductance	Drain - B+	745 μ H (Typ.)	100 kHz, 1 V

Table 3.

Layer	TERMINAL		WIRE	Turns	Isolation Layer
	Start Pin	End Pin			Turns
Primary Winding (Np1)	3	2	2UEW 0.22 * 1	36	2
Secondary (Ns1)	9	7	0.55 * 1	11	1
AUX Winding	5	4	2UEW 0.18 * 1	12	1
Secondary (Ns2)	8	6	0.55 * 1	11	1
Copper Shield	4	-		1.2	2
Primary Winding (Np2)	2	1	2UEW 0.22 * 1	35	3

*Copper shield is open loop and connect to ground.

TEST DATA

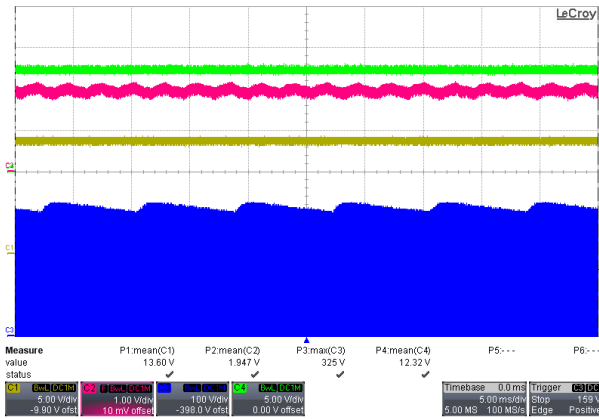


Figure 8. Operation, Full Load, 115 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: V_o)

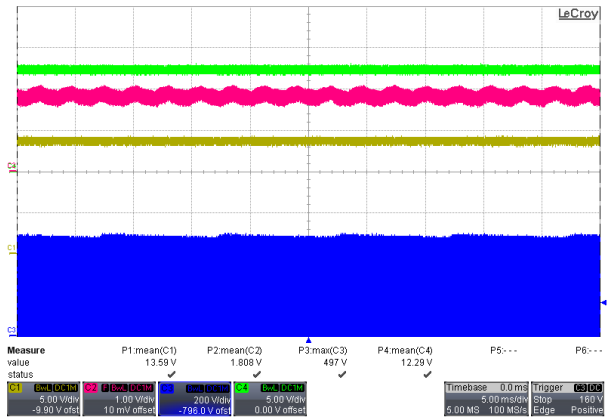


Figure 9. Operation, Full Load, 230 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: V_o)

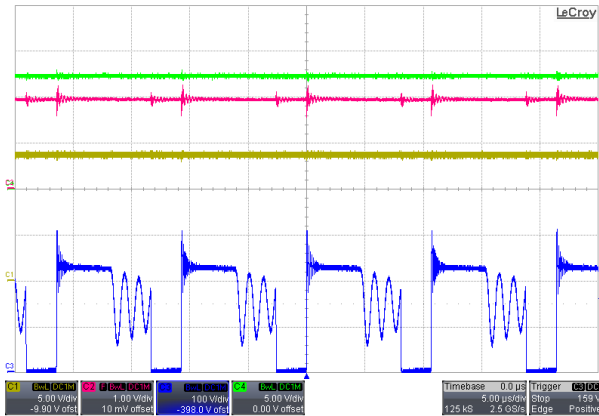


Figure 10. Zoom in Operation, Full Load, 115 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: V_o)

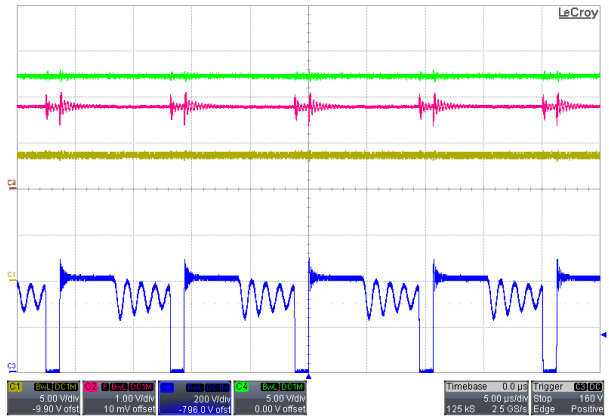


Figure 11. Zoom in Operation, Full Load, 230 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: V_o)

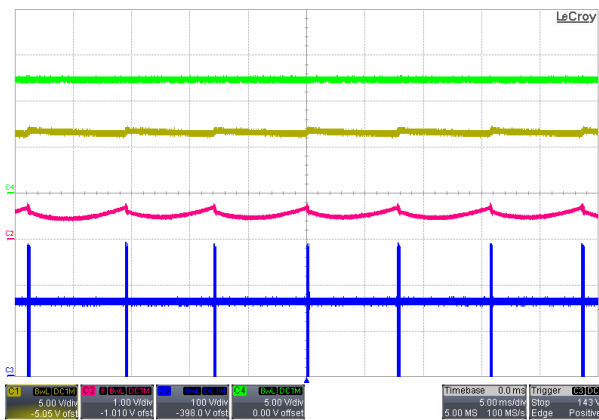


Figure 12. Operation, No Load, 115 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: V_o)

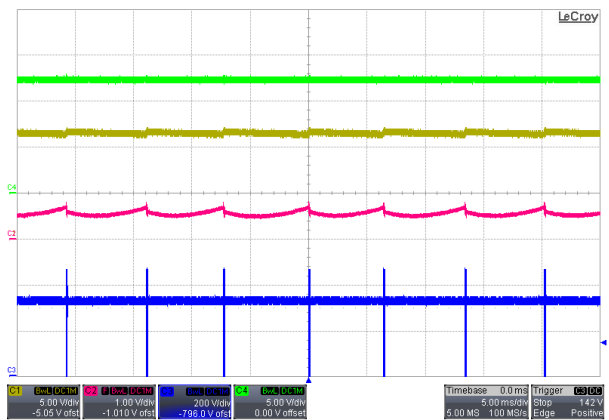


Figure 13. Operation, No Load, 230 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: V_o)

TEST DATA (Continued)

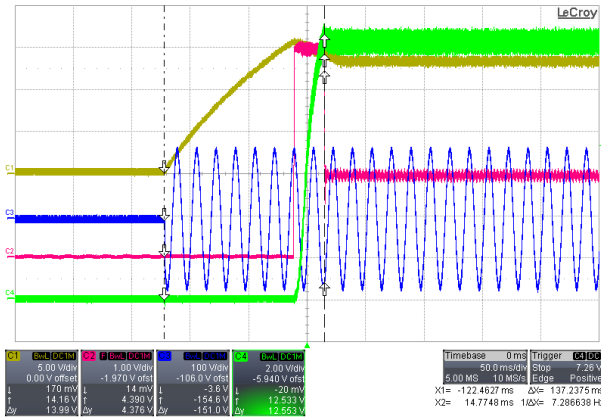


Figure 14. Ton On time, 115 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Vac, Ch4: Vo)

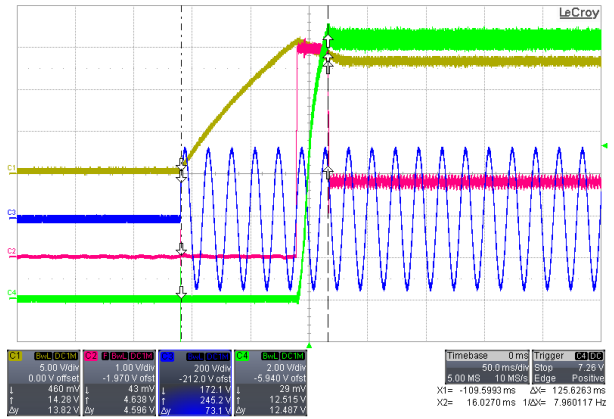


Figure 15. Ton on time, 230 Vac
(Ch1: V_{CC}, Ch2: COMP, Ch3: Vac, Ch4: Vo)

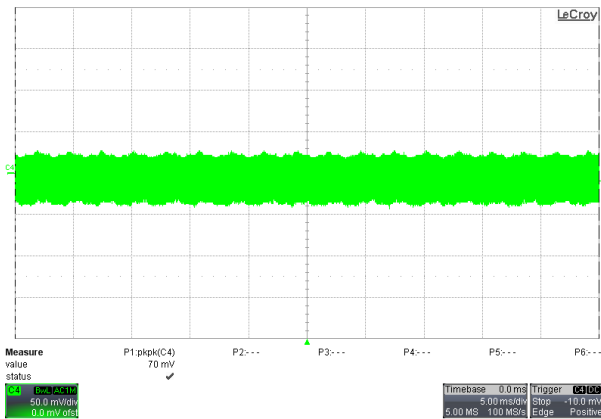


Figure 16. Output Ripple, Full Load, 115 Vac
(Ch4: V_O (AC))

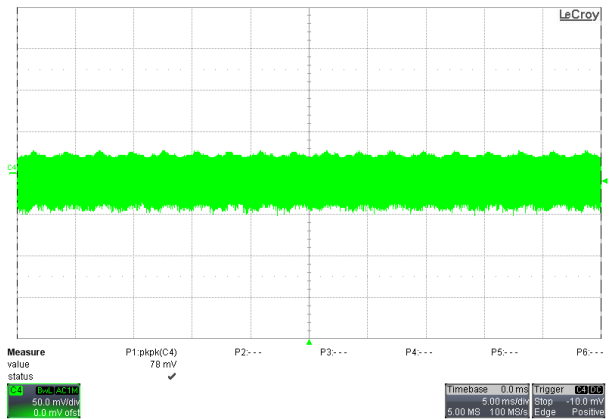


Figure 17. Output Ripple, Full Load, 230 Vac
(Ch4: V_O (AC))

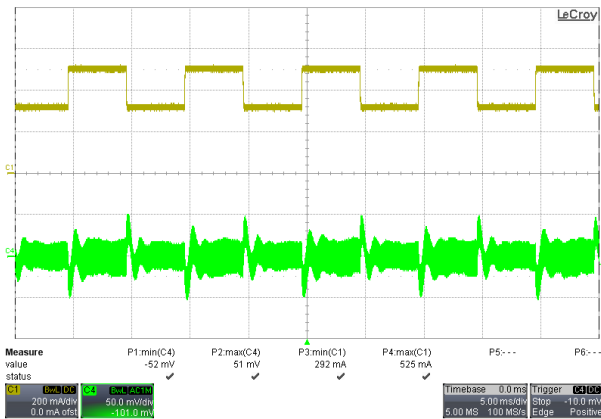


Figure 18. Dynamic Operation
(20%~80% of the Full Load, 5 ms Duty Cycle,
2.5 A/ μ s Rise/Fall Time), 115 Vac
(Ch1: Io, Ch4: Vo(AC))

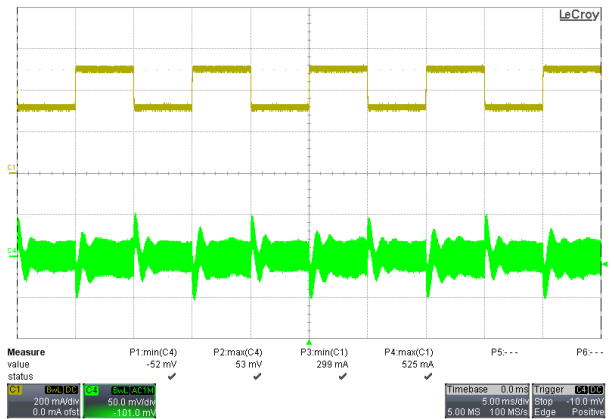


Figure 19. Dynamic Operation
(20%~80% of the Full Load, 5 ms Duty Cycle,
2.5 A/ μ s Rise/Fall Time), 230 Vac
(Ch1: Io, Ch4: Vo(AC))

TEST DATA (Continued)

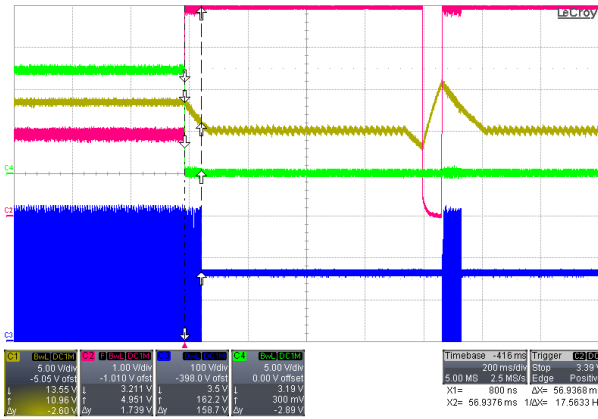


Figure 20. Output Short Triggers OLP, Full Load, 115 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

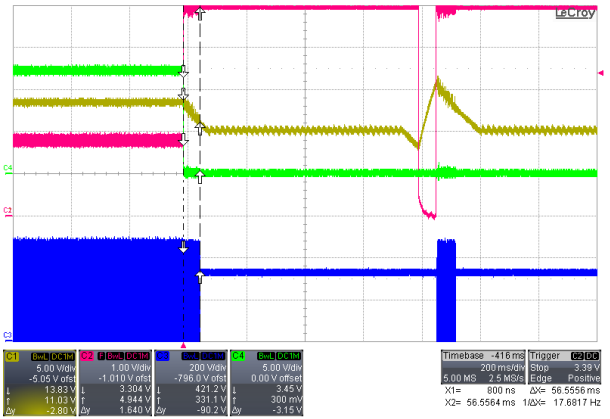


Figure 21. Output Short Triggers OLP, Full Load, 230 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

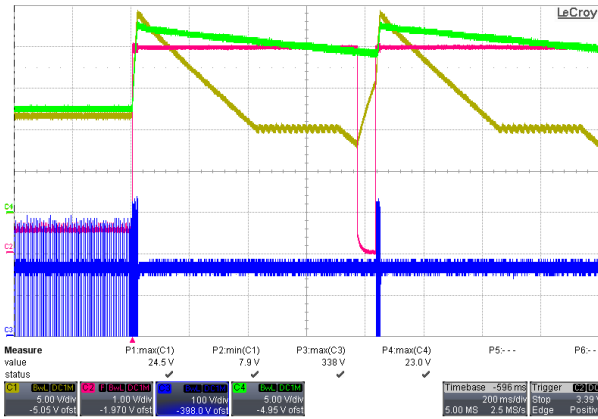


Figure 22. Short Photo Couple of Secondary Side to Trigger V_{CC} OVP, No Load, 115 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

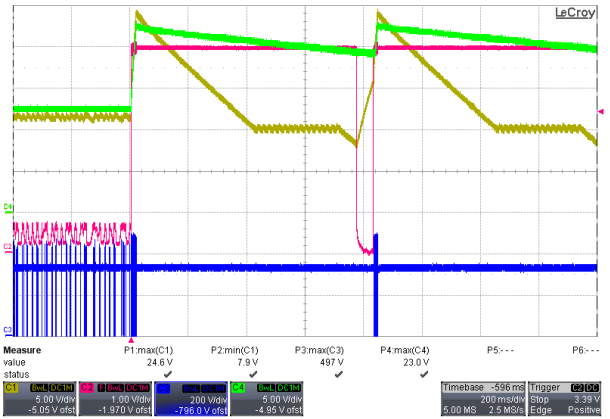


Figure 23. Short Photo Couple of Secondary Side to Trigger V_{CC} OVP, No Load, 230 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

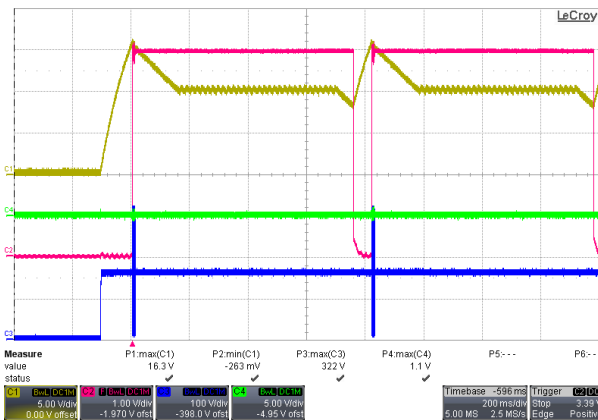


Figure 24. Short Output Schottky Diode to Trigger AOCP, Full Load, 115 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

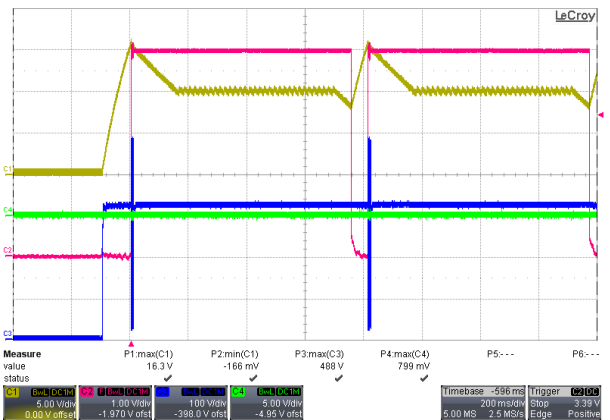


Figure 25. Short Output Schottky Diode to Trigger AOCP, Full Load, 230 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

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TEST DATA (Continued)

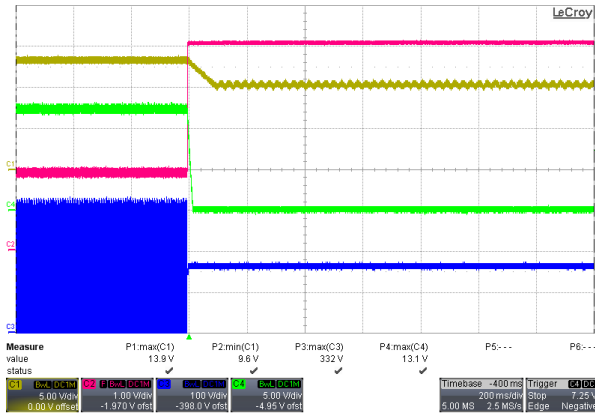


Figure 26. Heating on IC's Case to Trigger TSD, Full Load, 115 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

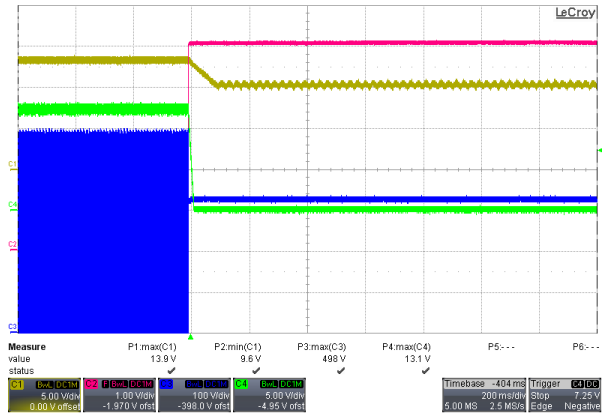


Figure 27. Heating on IC's Case to Trigger TSD, Full Load, 230 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

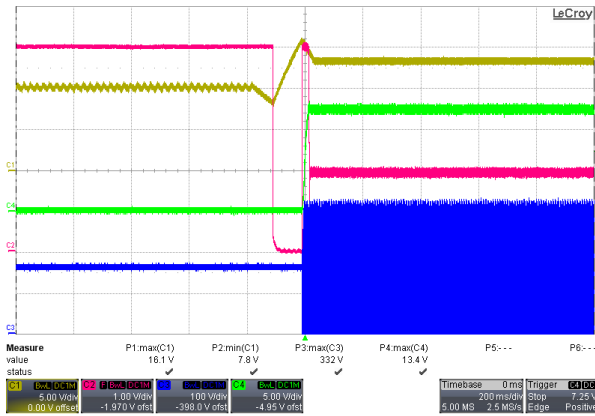


Figure 28. Remove Heating from IC's Case to Recover TSD Protection, Full Load, 115 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

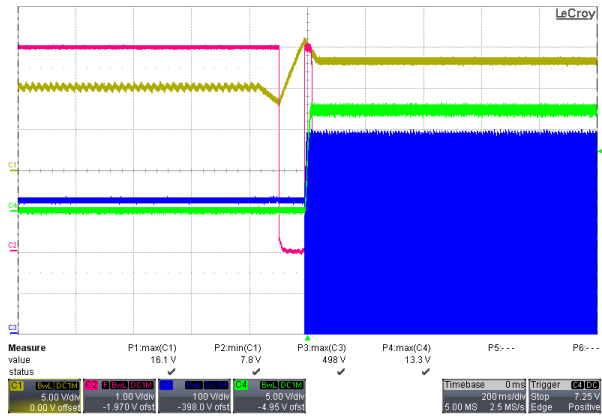


Figure 29. Remove Heating from IC's Case to Recover TSD Protection, Full Load, 230 Vac (Ch1: V_{CC}, Ch2: COMP, Ch3: Drain, Ch4: Vo)

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Table 4. BROWN IN/OUT

Behavior	Vin (Vrms)
Brown In	76
Brown Out	65

NOTE: Test condition is full load.
Gradually increase/decrease input AC by 1 V/step.

Table 5. NO-LOAD INPUT POWER CONSUMPTION

Input Voltage [Vac]	Power Consumption [mW]
115 Vac	24.18
230 Vac	39.50

NOTE: Test condition: Outputs are connected to electronic load, but loading is not applied. Input power is integrated over three minutes.

Table 6. EFFICIENCY

Input Voltage [Vac]	25% Load	50% Load	75% Load	100% Load	Avg.
115 Vac	86.91%	87.41%	87.46%	87.34%	87.28%
230 Vac	84.01%	85.57%	86.18%	87.25%	85.75%

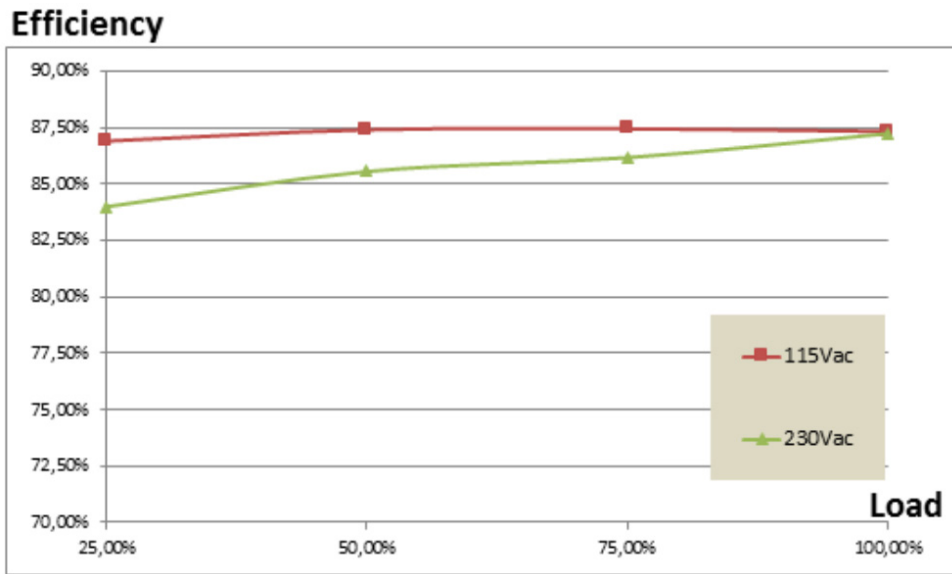


Figure 30. Board Efficiency

Table 7. LINE/LOAD REGULATION

Input Voltage [Vac]	85 Vac	115 Vac	230 Vac	265 Vac	Line Regulation (±)
Load	V _{OUT} (V)	V _{OUT} (V)	V _{OUT} (V)	V _{OUT} (V)	V _{OUT} (V)
0 W	12.389	12.387	12.386	12.385	0.016%
0.1 W	12.389	12.386	12.385	12.384	0.020%
0.25 W	12.388	12.385	12.384	12.383	0.020%
0.5 W	12.387	12.384	12.382	12.381	0.024%
25 %	12.379	12.378	12.375	12.374	0.020%
50 %	12.372	12.371	12.367	12.366	0.024%
75 %	12.365	12.364	12.360	12.358	0.028%
100 %	12.358	12.356	12.353	12.351	0.028%
Load Regulation (±)	0.125%	0.125%	0.133%	0.137%	

NOTE: Equation of line/load regulation is $\pm(\max - \min) / (\max + \min)$.
 Measured within load range shown in specification.

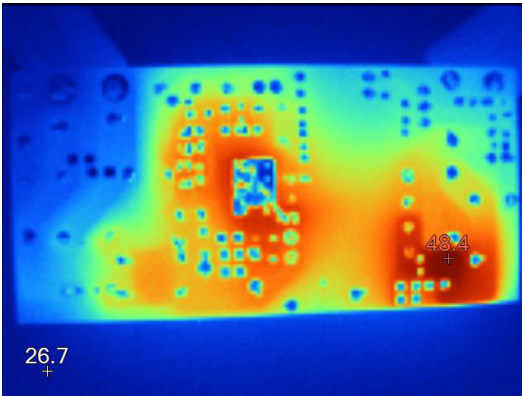


Figure 31. Temperature Checking on Bottom Side, Full Load, 115 Vac

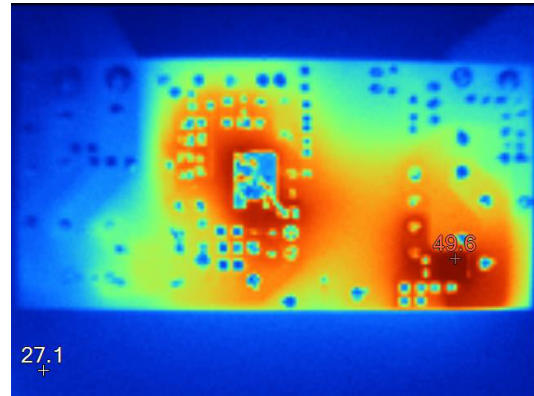


Figure 32. Temperature Checking on Bottom Side, Full Load, 230 Vac

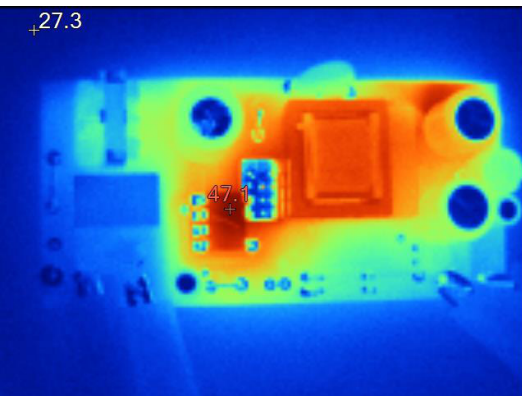


Figure 33. Temperature Checking on Top Side, Full Load, 115 Vac

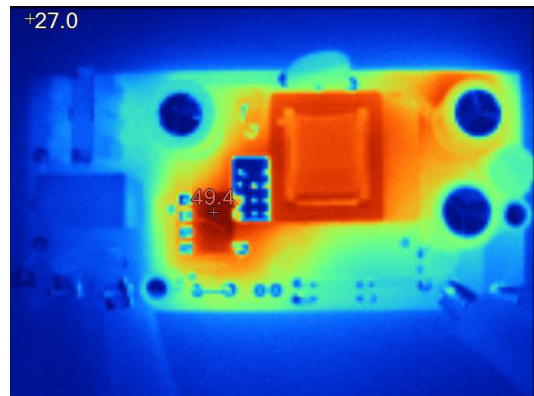
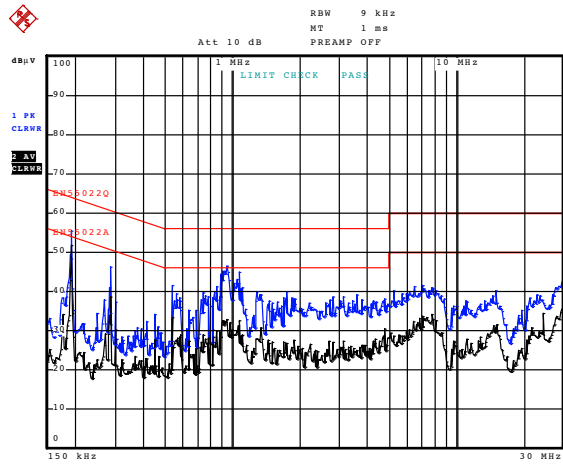
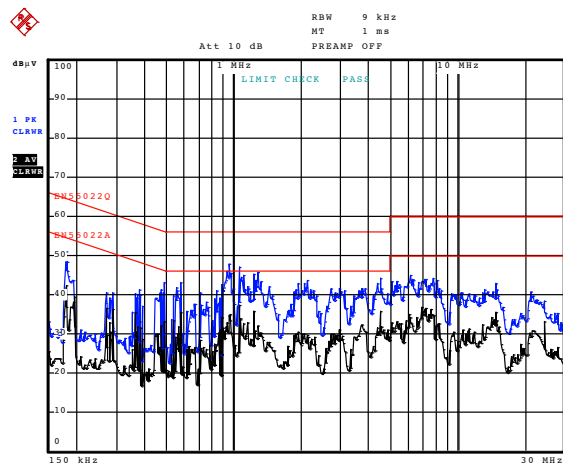


Figure 34. Temperature Checking on Top Side, Full Load, 230 Vac



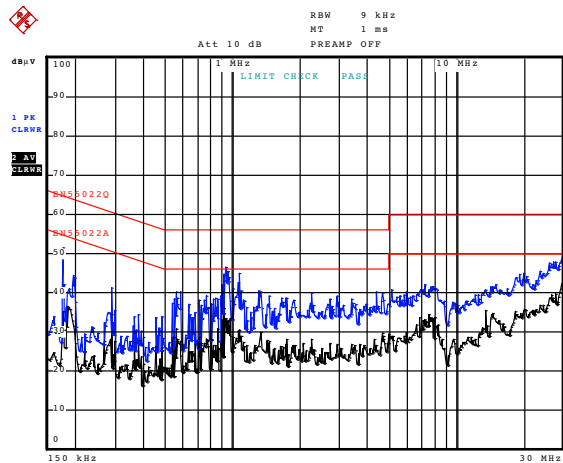
Date: 13.SEP.2018 19:05:49

Figure 35. Conducted EMI, 115 Vac, LINE



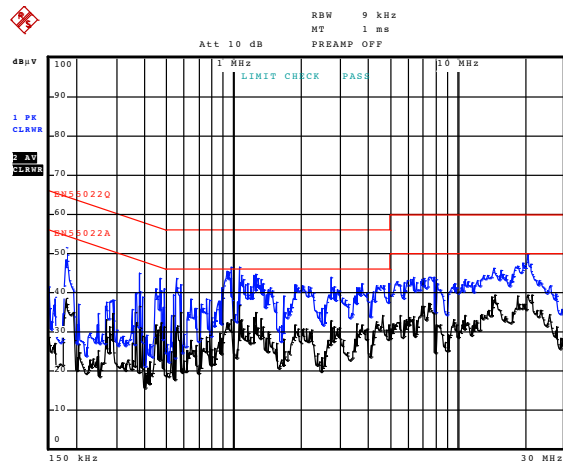
Date: 13.SEP.2018 19:08:09

Figure 36. Conducted EMI, 230 Vac, LINE



Date: 13.SEP.2018 19:06:53

Figure 37. Conducted EMI, 115 Vac, Neutral



Date: 13.SEP.2018 19:07:32

Figure 38. Conducted EMI, 230 Vac, Neutral

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BILL OF MATERIALS

Table 8. BILL OF MATERIALS

Parts	Qty	Description	Value	Tolerance	Footprint	Manufacturer	Manufacturer Part Number	Substitution Allowed	Pb-Free
C1	1	X2 Capacitor	0.33 μ F/275 V	\pm 10%	17 \times 7.5 \times 15.5 mm Pitch = 15 mm	CARLI	PX334K3ID1	Yes	Yes
C10, C17	2	MLCC X7R Capacitor	102 pF/50 V	\pm 10%	0805	Taiwan-Resister	CP102K050XRB	Yes	Yes
C13	1	MLCC X7R Capacitor	682 pF/50 V	\pm 10%	0805	Taiwan-Resister	CP682K050XRB	Yes	Yes
C15	1	MLCC X7R Capacitor	104 pF/50 V	\pm 10%	0805	Taiwan-Resister	CP104K050XRB	Yes	Yes
C1	1	X2 Capacitor	0.22 μ F/275 V	\pm 10%	P = 10 mm	CARLI	PX224K3IC5	Yes	Yes
C2	1	MLCC X7R Capacitor	102 pF/1 kV	\pm 10%	1206	KEMET	C1206C102KDRACTU	Yes	Yes
C14	1	Y1 Capacitor	222 pF/250 V	\pm 20%		UNIVERSE	CD12-E2GA222MYASA	Yes	Yes
C4	1	Electrolytic Capacitor	18 μ F/400 V		10 \times 20 mm	AISHI	EHL2GM180G200T	Yes	Yes
C6, C6A	2	Electrolytic Capacitor	470 μ F/25 V		10 \times 12 mm	CHEMI-CON	EKMG250ELL471MJC5S	Yes	Yes
C7	1	Electrolytic Capacitor	68 μ F/25 V	\pm 20%	5 \times 11 mm	Rubycon	25ZLH68M5X11	Yes	Yes
C16	1	Electrolytic Capacitor	22 μ F/50 V	\pm 20%	5 \times 11 mm	JACKCON	LHK	Yes	Yes
R14	1	Resistor SMD	47.5 k Ω	\pm 5%	0805	Taiwan-Resister	RP0847K5JR	Yes	Yes
R11, R17	1	Resistor SMD	5.1 k Ω	\pm 5%	1206	Taiwan-Resister	RP1205K1JR	Yes	Yes
R18	1	Resistor SMD	1 M Ω	\pm 5%	0805	Taiwan-Resister	RP0801MJR	Yes	Yes
R19	1	Resistor SMD	180 k Ω	\pm 1%	0805	Taiwan-Resister	RP08180KFR	Yes	Yes
R23	1	Resistor SMD	100 k Ω	\pm 5%	0805	Taiwan-Resister	RP08100KJR	Yes	Yes
R1, R2, R8	3	Resistor SMD	200 k Ω	\pm 5%	1206	Taiwan-Resister	RP12200KJR	Yes	Yes
R9	1	Resistor SMD	1 R	\pm 5%	1206	Taiwan-Resister	RP1201R0JR	Yes	Yes
R3, R21	1	Resistor SMD	0 R	\pm 5%	1206	Taiwan-Resister	RP12000JR	Yes	Yes
R22	1	Resistor SMD	22 M Ω	\pm 5%	1206	Taiwan-Resister	RP1222M0JR	Yes	Yes
D1	1	Fast Rectifier	600 V, 1 A		DO-214AC	ON Semiconductor	ES1J	Yes	Yes
D2	1	Zener Diode	7.5 V, 0.2 W		SOD-523F	ON Semiconductor	MM5Z7V5	Yes	Yes
D3	1	Fast Rectifier	200 V, 1 A		DO-214AC	ON Semiconductor	RS1D	Yes	Yes
D4	1	Jumper Wire	Short		5 mm			Yes	Yes
D5	1	Schottky Rectifier	120 V, 10 A		TO-277	ON Semiconductor	FSV10120V	Yes	Yes
L, N, 12V, GND	4	TEST PIN	Pin Ψ 2.2 \times 18.2 mm OEM-10		2.2 \times 18.2 mm	KANG YANG	SG004-05 Pin	Yes	Yes
F1	1	Fuse	FUSE CERAMIC 1 A/250 V SLOW		3.6 \times 10 mm		37SG	Yes	Yes
MOV	1	MOV	470 V	\pm 10%		THINKING	MOV-471KD10SBNL	Yes	Yes
NTC	1	Jumper Wire	short		7 mm			Yes	Yes
L1	1	Common-mode Choke	30 mH		UU9.8	SEN HUEI	TRN0330	Yes	Yes
L2	1	Inductor, Ferrite Core	1 μ H		DR 6 \times 8	WURTH	744772010	Yes	Yes
BD1	1	Bridge Rectifier	600 V, 1.5 A		SDIP-4	ON Semiconductor	DF06S	Yes	Yes
TX1	1	Transformer	745 μ H	\pm 5%	EE-19H-9P	SEN HUEI SWARM BOBBIN	TRN0369 SW-19AG	No	Yes

EVBUM2652/D

Table 8. BILL OF MATERIALS (continued)

Parts	Qty	Description	Value	Tolerance	Footprint	Manufacturer	Manufacturer Part Number	Substitution Allowed	Pb-Free
U1	1	PWM with Power SENSEFET			PDIP-7	ON Semiconductor	FSL518APG	No	Yes
U2	1	Opto Coupler	CTR = 80-160%		DIP 4-pin	ON Semiconductor	FOD817A	Yes	Yes
U3	1	Shunt Regulator	Adjustable, 2.5 V	1%	TO-92	ON Semiconductor	NCP431AVLPRAG	Yes	Yes
	1	PCB			38 x 80 mm		PLM0433V0	No	Yes
NTC, D4, F1	3	Teflon Tube	17L x 305 m					Yes	Yes

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